

ment and the uniform stress boundary conditions were considered at the end tab surfaces. The results under the two different boundary conditions are practically the same within the gauge length section and around the tab tip. Under the end tab region different boundary conditions (stress vs displacement) result in significantly different results. For a thicker IITRI specimen the stress concentrations and the stress profiles obtained by the two different boundary conditions are considerably different. Since there is no stress concentration in the gauge length section of the specimen, the compressive modulus can be measured using the Celanese or IITRI specimens. However, a preliminary study has shown that the apparent strengths determined by these test methods are significantly lower than those obtained from face-supported specimens.<sup>9</sup> This suggests that stability could be a problem for the Celanese and IITRI specimens. Additional stability analysis is needed to confirm this result.

### Acknowledgment

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## Errata

### Numerical Simulation of the Convective Instability in a Dump Combustor

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FIGURE 7b was inadvertently omitted from this paper and should have appeared with Fig. 7a as follows.

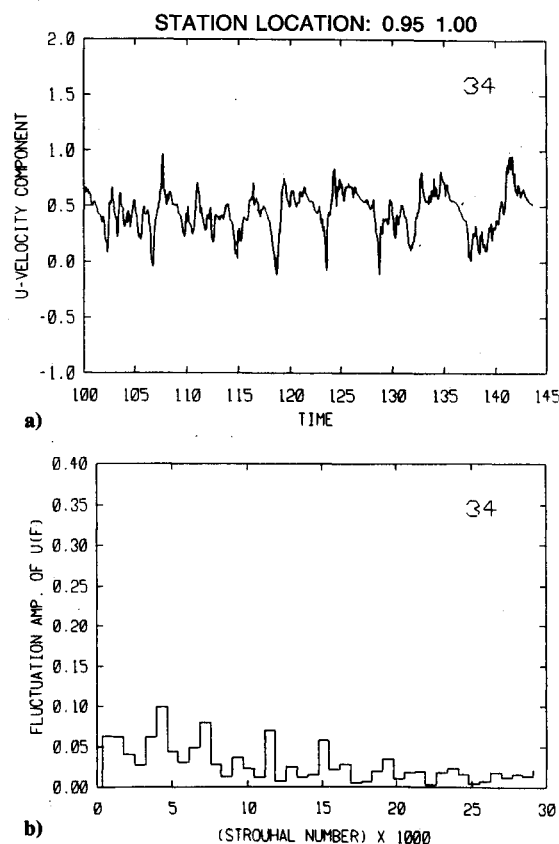


Fig. 7 Velocity fluctuation a) and frequency spectrum b) for cavity with  $L/D = 2.0$ ,  $L/\theta_0 = 1000$  at  $x/D = 0.95$ ,  $y/D = 1.0$ .